

SOIL PROPERTIES FROM IN SITU TESTS by "TRIANGULATION"

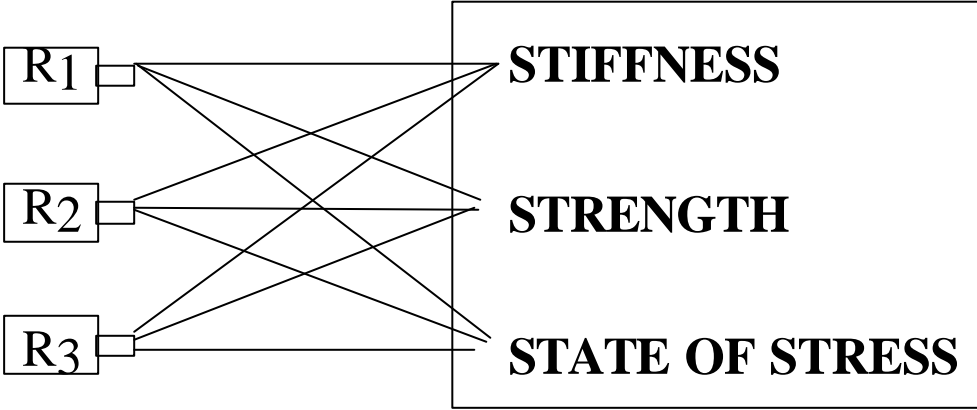
- UNABLE MEASURE IN SITU **PURE** SOIL PROPERTIES
- RESPONSES** IN SITU: **MIXED FUNCTION** *PURE* S.P.
- TO ISOLATE *PURE* S.P. : "TRIANGULATION"
- say **DOMINANT STIFFNESS, STRENGTH, STATE STRESS**
- NEED 3 INDEP. IN SITU RESPONSES R1, R2, R3

$$\begin{aligned}
 R_1 &= f_1 (M, \text{Strength}, \sigma_h) \\
 R_2 &= f_2 (M, \text{Strength}, \sigma_h) \\
 R_3 &= f_3 (M, \text{Strength}, \sigma_h)
 \end{aligned}$$

**INVERT
MATRIX
GET**

$$\begin{aligned}
 M &= g_1 (R_1, R_2, R_3) \\
 \text{Strength} &= g_2 (R_1, R_2, R_3) \\
 \sigma_h &= g_3 (R_1, R_2, R_3)
 \end{aligned}$$

TRIANGULATION \approx 3-Chromia to re-create colors



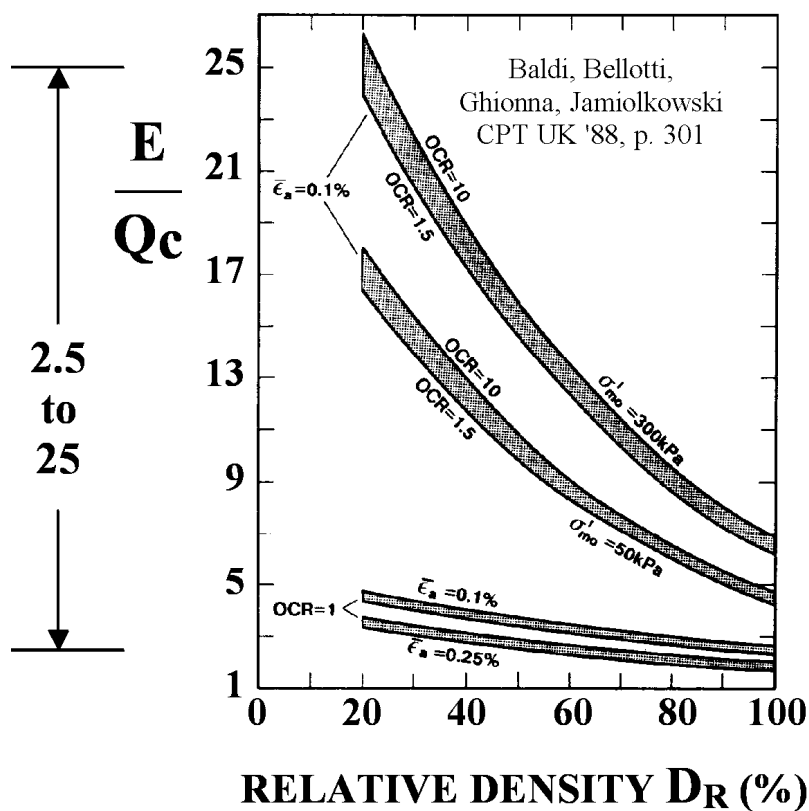
DMT is a TWO-PARAMETER TEST

Makes a lot of difference compared with 1-parameter tests as CPT or SPT (3 would be better, but diminishing returns...

Moreover 3rd parameter would be valuable if truly independent - DMT tip **q_D** not sure...)

1-parameter test \Rightarrow wide UNCERTAINTY

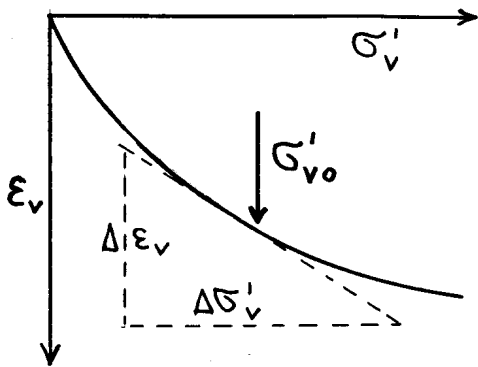
- 1 information : NO MATRIX to INVERT
- $E=2.5$ to $25 Q_c$ (factor 10) = $f(D_r, OCR-S_h)$
- Impossible get 3 *unknowns* (E , D_r , OCR) from just 1 information (Q_c)



- If we adopt ave. $E=7 Q_c$, E could be off (settlements) by factor 3 (wide).
- Jamiolkowski et al. conclude (Isopt-1, '88, Vol. 1, p.263) : "w/o Stress History, impossible to select reliable E (or M) from Q_c "

1. Definition of M (no ambiguity)

$$M = E_{oed} = 1/m_v = \Delta\sigma'_v / \Delta\varepsilon_v \text{ (at } \sigma'_{vo}\text{)}$$



Vert. drained confined tangent (at σ'_{vo}) modulus

Name : E_{oed} OK, traditionally measured by oedometer.

Improper if not by oed (correlations). Hence "M", but same.

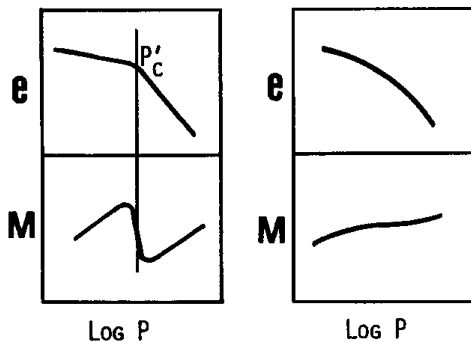
Usual range M_{DMT} **4 - 4000 bar**

2. M for what settlement (initial, 1^{ry}, 2^{ry}) ?

M is just for **primary**. Correlations were established by calibrating vs E_{oed} (1-D). M_{DMT} **must be treated as if by oedometer**.

Use same methods as with oedometers, including, if applicable, usual corrections (depth, shape, rigidity, possibly Skempton-Bjerrum).

3. May use M = constant if Ds'_v large ?



If $\Delta\sigma'_v$ large : σ'_v may exceed p_c . (?)

Many structured NC clays (eg some Canadian) : sharp break in e - $\text{log } p$ curve \Rightarrow marked drop in M at p_c .

There M_{DMT} may be too high.

But in many common clays, (in most sand?) M across p_c mild

fluctuation, hence $M = \text{const.} \approx \text{OK}$